



**Design point**

**1. Selection of switching device:**

Thyratron is used in general for the switch of high voltage and high current. As to the thyratron as satisfying to Table 2, we have chose the big tube, CX-1720MN which has a effective result after discussion with EEV(Maker of thyratron).

**Table 2**  
Parameter for operating switching device

		Max.rating
PFN charging voltage [KV]	33	50
PFN peak current [A]	1080	5000
PFN average current [A]	14.4	25
Recovery time [uS]		25

**2. Use of command charging system**

One of specifications in thyratron, there is problem of recovery time. In order to recover thyratron, it should be kept over 25uS at condition of Anode voltage below 100V after stopping thyratron. Therefore, thyristor is used for the switch in order to turn on or turn off the charging voltage. Thyratron surely was recovered by trigger timing as Fig.3.

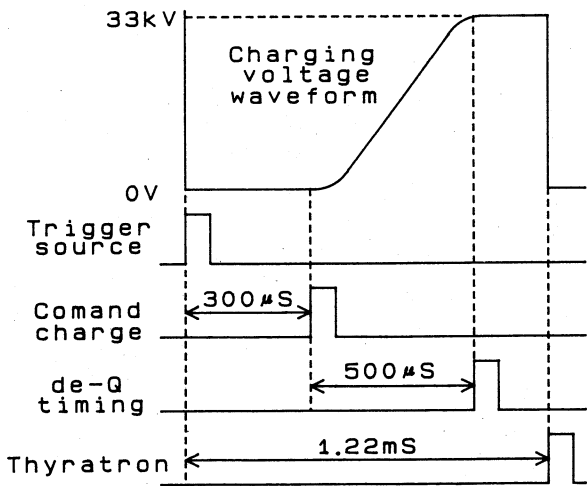


Fig.3 Block diagram of trigger timing

**3. Selection of SCR thyristor for hold off of command charging system**

The SCR thyristor is required to satisfy Table 3, and so there are two important an issue. One is the research for the SCR break down voltage (3-1). The other is the SCR gate trigger system (3-2).

**Table 3**  
Parameter of thyristor

PFN charging voltage [KV]	33
PFN charging	
Peak current [A]	50
RMS current [A]	30
Average current [A]	16

**3-1. Research for the SCR break down voltage**

In case of high speed thyristor, the peak repetitious opposite voltage is about 2500V at the maximum, if required as Table 3, it is better to use in series /30pcs according to the device of dilating break down voltage, and then we use 6pcs per 1 stack, ie using 5 stack. And also using high speed thyristor(turn off time <40uS) was adopted in order to keep the precision of charging voltage.

**3-2. SCR gate trigger system**

It is required to put the reliable gate trigger in order to operate surely all of SCR/30pcs at the same time without failure, and then it is operate by the insulated pulse transformer which is able to endure 40kV. Fig.4 shows the configuration of the insulated pulse transformer for SCR gate trigger unit.

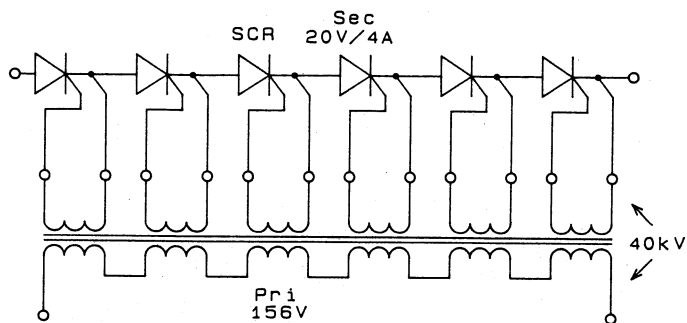


Fig.4 Configuration of the insulated pulse transformer for SCR gate trigger unit

**4. Treatment for noise**

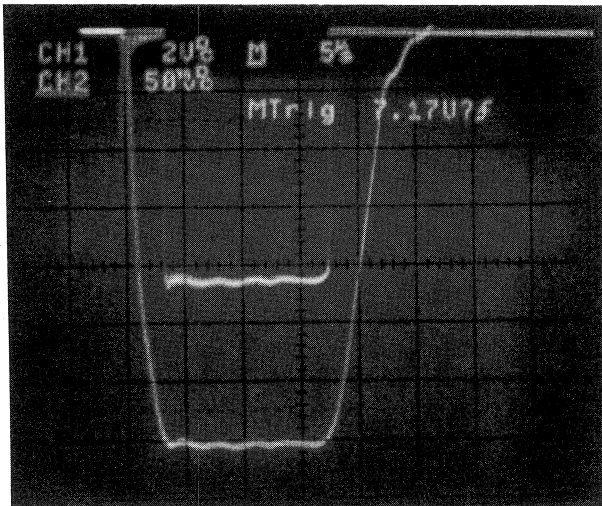
With regard to noise treatment, we bind the sheet copper (width 365mm, thickness 0.1mm) to bottom of enclosure and between enclosure and klystron. Then we have succeeded to operate surely this equipment without any trouble.

**Test results**

Picture 1 through 3 shows the wave form at each position for this line-type pulse modulator, and then these wave form have indicated really steady operation without disturbance due to noise.

Photo.1

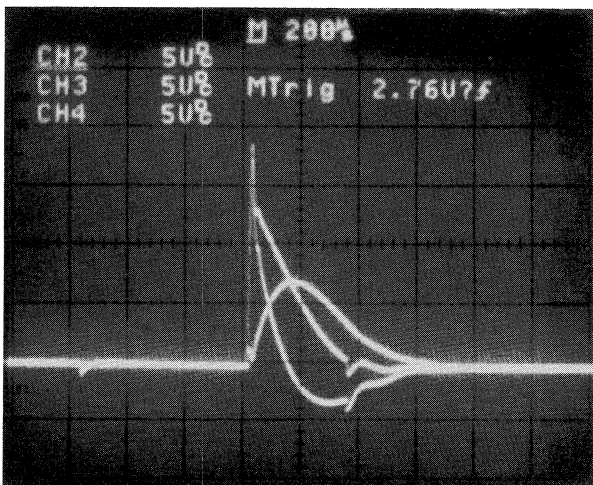
Up rf output power 5.5MWpeak  
Down Klystron beam voltage 140kVpeak



Up 50mV/div 5uS/div  
Down 20kV/div 5uS/div

Photo.2

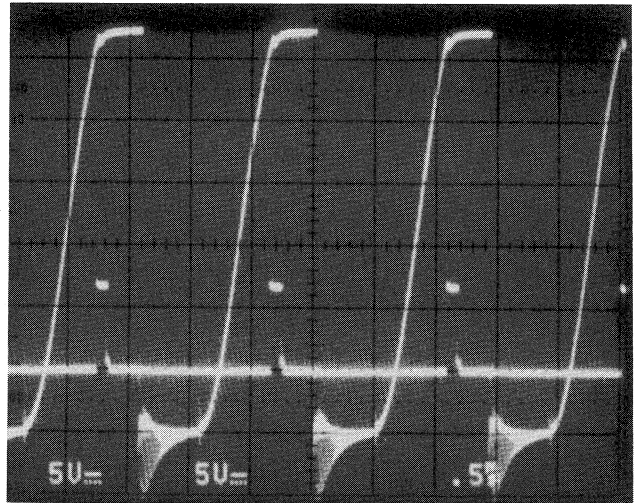
Up de-Q R current 300Apeak  
Middle de-Q current 800Apeak  
down de-Q C current 800Apeak



Up/Middle/Down 200A/div 200uS/div

Photo.3

Up Charging voltage 33kV  
Down de-Q timing of trigger



Up 5kV/div 500uS/div  
Down 5V/div 500uS/div

**Conclusion**

We have succeeded to develop the pulse power supply at the first achievement in the world which has gained pulse width 14uS and the pulse repetition 700pps.

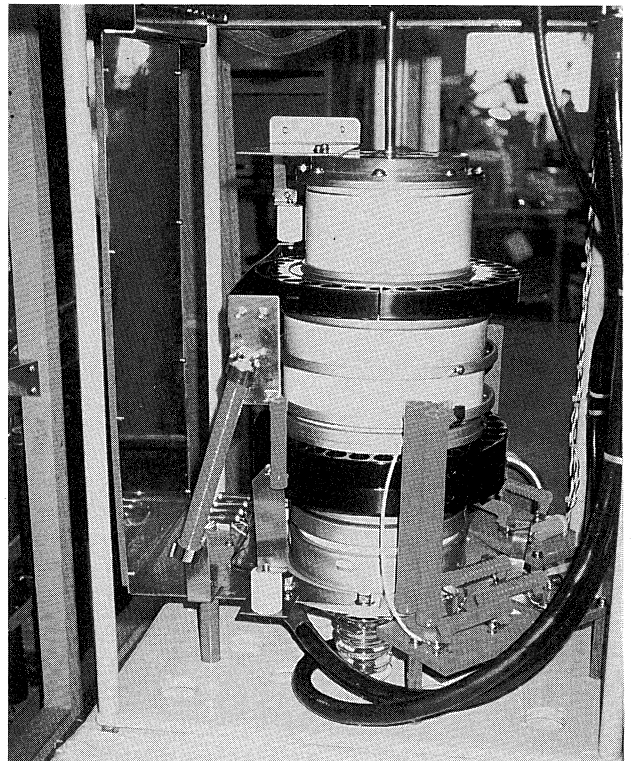


Photo.4 Thyatron unit for forced oil cooling